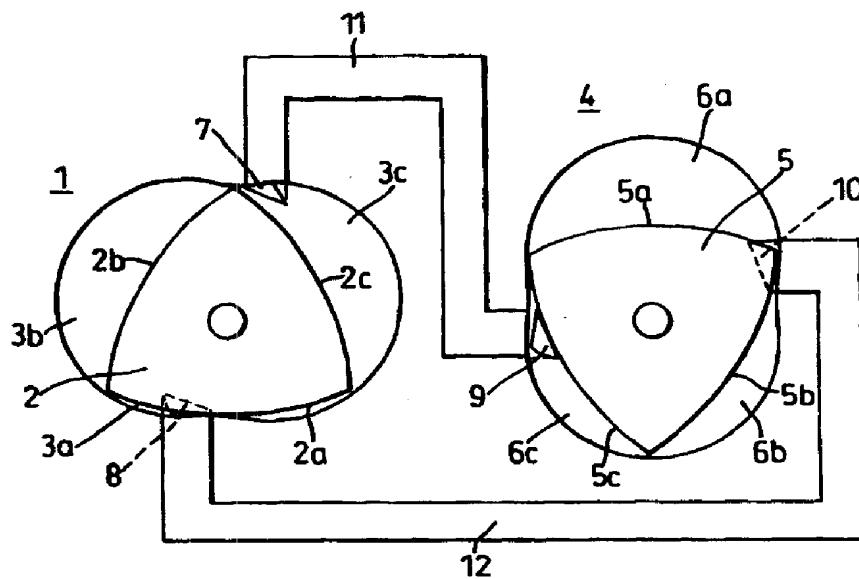




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(54) Title: IMPROVEMENTS RELATING TO ROTARY PISTON MACHINES



(57) Abstract

A rotary piston machine adapts the Stirling principle and can operate as an engine or a heat pump. Two variable volume units (1, 4) have n-lobed chambers (3, 6) rotatable about a common axis at a first speed. Each chamber contains an (n+1) sided piston (2, 5), these being rotatable about a different common axis at a different second speed, and cooperating with the lobes to form expanding and reducing sub-chambers. The first to second speed ratio is (n+1):n ducts (10, 11) incorporating regenerators provide intercommunication between the chambers (3, 6) and are open and closed by the relative piston rotation to exchange fluid or vapor between units. Heating may be provided for one unit, the expansion unit (1), and cooling for the other, the compression unit (4), and the ducts can also incorporate heating and cooling means.

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Improvements relating to Rotary Piston Machines

This invention relates to rotary piston machines. It is concerned with an adaptation of the Stirling principle, with multi-sided rotary pistons operating in chambers with 5 epitrochoidal lobes, the working fluid or vapour undergoing closed thermodynamic cyclic processes. The machine may operate as an engine or as a heat pump.

According to the present invention there is provided a fluid or vapour rotary piston machine including two 10 variable-volume units, each unit having a rotary multi-lobed epitrochoidal chamber and a multi-sided rotary piston therein forming a plurality of individual sub-chambers by its co-operation with the periphery of the associated chamber, the number $(n+1)$ of piston sides being greater by 15 one than the number (n) of epitrochoid arcs, wherein the two chambers are constrained to rotate at a first common speed about a first effective common axis while the two pistons are constrained to rotate at a second common speed about a second effective common axis, the ratio of first to 20 second common speeds being $n+1:n$, wherein each chamber has a plurality (n) of dual-function ports enabling connection between the chambers via ducts, and wherein said ducts each contain a regenerator, enabling one variable-volume unit to perform intake, expansion and exhaust, while the other unit 25 performs intake, compression and exhaust, as a result of the relative rotation and port positions.

Preferably, the chambers will be co-axial, as will be the rotors. That simplifies construction. But they could,

in theory, be on different axes but coupled to rotate in liaison. The term "effective" is intended to cover this alternative.

Heating means may be provided for the variable-volume unit which performs the expansion processes, and there could be further heating means between each said regenerator and the variable-volume unit which performs the expansion processes.

Cooling means may also be provided for the variable-volume unit which performs the compression processes, and there could be further cooling means between each said regenerator and the variable-volume unit which performs the compression processes.

In the preferred form n=2, so that there are three sided pistons operating in double-lobed chambers.

The expansion unit which may, but not necessarily, be heated, will have its ports disposed in such a way that the chambers formed therein are increasing in volume generally when not in communication with a port and decreasing in volume generally when said chambers are in communication with a port. The other, compression unit which may, but not necessarily, be cooled, will have its ports disposed in such a way that the chambers formed therein are decreasing in volume generally when not in communication with a port, and increasing in volume generally when said chambers are in communication with a port. Work processes thus occur in chambers isolated from port openings, while the transfer of working fluid or vapour occurs between a pair of chambers

each in communication with ports opening to a common duct. If high-grade heat transfer is accomplished to the working fluid or vapour flowing to, from or contained within, the expansion unit, while low-grade heat transfer is accomplished from the working fluid or vapour flowing to, from, or contained within, the compression unit, the machine behaves as an engine, with mechanical work output. If mechanical work is applied to the rotating components, but low-grade heat transfer is accomplished to the region of the expansion unit while high-grade heat transfer occurs from the region of the compression unit, the machine behaves as a heat pump or refrigerating machine.

For a better understanding of the invention, reference will now be made by way of example, to the accompanying drawings, in which:

Figures 1, 2, 3, 4 and 5 are schematic diagrams showing the relative positions of expansion and compression units of a rotary piston machine at intervals during a cycle of rotation, and

Figure 6 is a diagrammatic cross-section through a preferred embodiment of the machine.

An expansion unit 1 has a rotary piston 2 contained in a chamber 3 and a compression unit 4 has a rotary piston 5 contained in a chamber 6. Each piston 2 and 5 is of flat, generally equilateral triangular form, but with the sides of the triangle convex and arcuate. Each chamber 3 and 6 is also flat, closely to confine the faces of the piston, and is of two-lobed epitrochoidal form. The chambers thus have

major and minor axes intersecting at right angles at their centres. The two units 1 and 4 are rigidly linked to rotate about a common axis through their centres in the same direction and at the same speed, the major axes of the chambers 3 and 6 being at 90° to each other. The two rotary pistons 2 and 5 are also rigidly linked to rotate about a common axis through their centres in the same direction and at the same speed, this being two thirds the speed of rotation of the chambers 3 and 6. The arcuate sides 2a, 2b 5 and 2c of the piston 2 are disposed at 180° to the counterpart sides 5a, 5b and 5c of the other piston 5. The sides of the pistons 2 and 5 co-operate with the profiles of the respective chambers 3 and 6 to form sub-chambers 3a, 3b 10 and 3c and 6a, 6b and 6c, of variable volume and shape in 15 operation, as described below.

Ports 7 and 8 in the expansion unit 1 are diagonally opposite each other and offset 30° in the direction of motion (clockwise as seen in Figures 1 to 5) from the minor axis of the chamber 3. Corresponding ports 9 and 10 are 20 similarly disposed in the compression unit 4, but are offset by 30° in the direction opposite that of rotation from the minor axis of the chamber 6. This positioning ensures that during operation a port, 7 or 8, is about to open to a sub-chamber when that sub-chamber is at maximum volume in the 25 expansion unit 1. Similarly, a port, 9 or 10, has just closed to a sub-chamber when that sub-chamber is at maximum volume in the compression unit 4. The expansion unit port 7 is linked by an interconnecting duct 11 to the compression

port 9 diagonally opposite with reference to the axis of rotation of the units 1 and 4, while the expansion unit port 8 is similarly linked by an interconnecting duct 12 to the compression unit port 10. These ducts each contain a 5 regenerator (not shown).

The sequence of operation is as follows:

In Figure 1, heated working fluid or vapour occupies the sub-chamber 3a, which is at minimum volume and is open, via the port 8, to the duct 12. The sub-chamber 3b is 10 isolated and increasing in volume. The sub-chamber 3c is decreasing in volume, thereby expelling working fluid or vapour via the port 7, through the duct 11. The fluid or vapour is giving up, in the case of an engine, or taking up, in the case of a heat pump, heat within the regenerator in 15 that duct 11. Cooled working fluid or vapour occupies the chamber 6a which is at maximum volume, isolated, and about to start its compression cycle. The sub-chamber 6b is in its compression cycle, is decreasing in volume and isolated. The sub-chamber 6c is increasing in volume and is open, via 20 the port 9, to the duct 11. It is therefore receiving the working fluid or vapour from the sub-chamber 3c. The port 10 is closed by the piston 5.

In Figure 2 the pistons 2 and 5 have rotated clockwise by 30° and the chambers 3 and 6 by 45° . The sub-chamber 3a 25 is increasing in volume and accepting working fluid or vapour, via the port 8, from the duct 12 and from the sub-chamber 6b, which continues to decrease in volume and now communicates with the port 10. The sub-chamber 3b continues

to increase in volume, with the isolated heated working fluid or vapour therein being expanded, while the transfer of working fluid or vapour continues from the sub-chamber 3c to the sub-chamber 6c via the port 7, the duct 11, and the 5 port 9. The cooled working fluid or vapour in the sub-chamber 6a remains isolated and is compressed as the volume of that sub-chamber decreases.

In Figure 3 the pistons have rotated through 60° from their initial positions and the chambers by 90°. The sub-chamber 3a continues to increase in volume, but the piston 2 closes the port 8, thereby terminating the ingress of working fluid or vapour, whereupon the expansion process commences within that sub-chamber. The sub-chamber 3b has attained its maximum volume, and the heated working fluid 15 therein has reached the end of its expansion process, while the sub-chamber 3c continues to decrease in volume with the egress of working fluid or vapour, via the port 7, the duct 11 and the port 9 to the compression unit 4. The cooled working fluid continues to be compressed in the isolated 20 sub-chamber 6a as the volume therein decreases. The sub-chamber 6b is at minimum volume and open, via the port 10, to the duct 12, but the working fluid or vapour ceases to flow due to the closure of the port 8. The sub-chamber 6c continues to increase in volume and to accept the working 25 fluid or vapour, via the port 9, from the sub-chamber 3c.

In Figure 4 the pistons 2 and 5 have moved on another 30° and the chambers 3 and 6 another 45°. The sub-chamber 3a is isolated and increasing in volume, with the heated

working fluid therein continuing its expansion process. The sub-chamber 3b now communicates with the port 8 as that is uncovered by the piston 2 and, since that sub-chamber is decreasing in volume, the working fluid or vapour therein is 5 forced out into the duct 12. The sub-chamber 3c continues to decrease in volume, and transfer of working fluid or vapour, via the port 7, the duct 11 and the port 9, continues to the compression unit 4. The sub-chamber 6a remains isolated and decreasing in volume, with the cooled working fluid or 10 vapour therein continuing its compression process. The sub-chamber 6b is now increasing in volume and, due to its communication with the port 10, accepts the working fluid or vapour from the sub-chamber 3b via the duct 12. The sub-chamber 6c continues to increase in volume and the ingress 15 of working fluid or vapour continues, via the port 9 and the duct 11, from the expansion unit 1.

In Figure 5 the pistons are 120° from their original positions and the chambers 180° from theirs. The sub-chamber 3a continues to increase in volume, with the heated, 20 isolated working fluid therein continuing its expansion process. The sub-chamber 3b continues to decrease in volume, with its working fluid or vapour passing via the port 8, the duct 12, and the port 10 to the sub-chamber 6b which is increasing in volume. The sub-chamber 3c is at minimum 25 volume and open, via port 7, to the duct 11, but the compression unit piston 5 has closed the port 9, and so the working fluid or vapour ceases to flow. The sub-chamber 6a is still isolated and decreasing in volume, with the cooled

working fluid therein at the end of its compression process. The sub-chamber 6b continues to accept the transferred working fluid or vapour from the expansion unit 1. The sub-chamber 6c, now isolated due to the closure of the port 9, 5 is at maximum volume with the working fluid or vapour therein at the commencement of its compression process. The situation within the machine is now similar to that of Figure 1, although the various bodies of working fluid or vapour occupy different spaces to those in the earlier 10 diagram.

Consider the body of cooled working fluid in the sub-chamber 6a in Figure 1 at the commencement of its compression process. As the units 1 and 4 rotate through 180° and the rotary pistons 2 and 5 rotate through 120° , the 15 relative rotor rotation will be 60° in the opposite direction. This finds the body of fluid in sub-chamber 6a at the end of its compression process in a similar situation to that of the cooled working fluid or vapour in the sub-chamber 6b in Figure 1. After a further 30° of relative 20 rotor rotation (corresponding to the Figure 3 positions) the sub-chamber 6a will be at minimum volume, and the major proportion of the working fluid or vapour that was therein will have transferred to the sub-chamber 3c via the port 9, the ducts 11 and the port 7, absorbing, in the case of an 25 engine, or rejecting, in the case of a heat pump, heat during its passage through duct 11. At this point, where the total relative rotor rotation is 90° , the piston 2 will have passed the port 7. The expander sub-chamber 3c allows

expansion of the heated working fluid or vapour therein until a further 60° of relative rotor rotation has occurred (making the total 150°), when the sub-chamber 3c is at maximum volume. Further rotation uncovers the port 8,
5 allowing egress of heated working fluid or vapour via the duct 12, in which it is cooled in the case of an engine, or heated in the case of a heat pump. It then enters the sub-chamber 6c via the port 10, this transfer process occurring over a further 90° of relative rotor rotation, the total
10 then being 240° , when the sub-chamber 3c will be at minimum volume. The piston 5 now covers port 10 and the thermodynamic cycle involving this particular body of working fluid or vapour is repeated.

The processes may be tabulated over 360° of relative
15 rotor rotation, corresponding to 720° of piston rotation and 1080° of chamber rotation, as set out below in Table 1.

The closed thermodynamic cycle described above occurs and repeats, with phase displacement, with four main bodies of working fluid or vapour. In Figure 1, these are located
20 in sub-chamber 6a at the commencement of compression, in sub-chamber 6b towards the end of compression, in sub-chambers 3c and 6c and duct 11 undergoing regenerative transfer, and in sub-chamber 3b undergoing expansion. The residual working fluid or vapour in sub-chamber 3a is
25 awaiting mixing with the main body of working fluid or vapour in the sub-chamber 6b. It will be noted that work processes in both the expansion and compression units are of equal duration, namely 60° of relative rotor rotation.

Working fluid or vapour regenerative transfer from the compression unit 4 to the expansion unit 1 is always to a sub-chamber of dissimilar designation, that is, 6a to 3c, 6b to 3a and 6c to 3b, and is of short duration, namely 30° of 5 relative rotor rotation. Working fluid or vapour regeneration transfer from the expansion unit 1 to the compression unit 4 is always to a sub-chamber of similar designation, that is, 3a to 6a, 3b to 6b and 3c to 6c, and is of long duration, namely 90° of relative rotor rotation. 10 If the units 1 and 4 are of equal size, which is not a necessity, the geometry ensures that this latter transfer occurs under constant summed volume.

The regenerative transfer of any one main body of working fluid or vapour is always accomplished alternately 15 between the two ducts 11 and 12. That is, transfer from one unit to the other via one duct is always followed by the return transfer via the other duct. Because of the pairings of sub-chambers during those transfers, any one main body of working fluid or vapour will eventually be transported 20 through every sub-chamber within the machine, allowing mass and energy balances of the working fluid or vapour to be attained rapidly.

The route followed by one main body of working fluid or vapour may be tabulated over 720° of relative rotor 25 rotation, corresponding to 1440° of piston rotation and 2160° of housing rotation, as shown below in Table 2. The main body of working fluid or vapour under study in that table is that which appears in sub-chamber 6a in Figure 1,

at the start of its compression process. It can be seen to undergo three complete thermodynamic cycles before it returns to that sub-chamber 6a, after passing through all the other sub-chambers of the machine. A second main body of 5 working fluid or vapour which appears in sub-chamber 6b in Figure 1, undergoing its expansion process, will follow an identical route to that shown in Table 2, with a phase displacement of +360° relative rotor rotation from that shown in Table 2. A third main body of working fluid or 10 vapour which appears in sub-chamber 6b in Figure 1, towards the end of its compression process, will follow a similar route, but with the ducts interchanged so that expansion unit to the compression unit transfers are made via the duct 11 whilst the reverse transfers are made via the duct 12, 15 with a phase displacement of +180° relative rotor rotation from that shown in Table 2. The fourth main body of working fluid or vapour which appears in sub-chambers 3c and 6c and duct 11 in Figure 1, undergoing regenerative transfer to the compression unit, will follow an identical route to that of 20 the third main body of fluid or vapour, with a phase displacement of -180° relative rotor rotation from that shown in Table 2. The machine therefore provides for a total of twelve thermodynamic cycles over the period defined by 25 1440° of piston rotation, corresponding to 2160° of chamber rotation and 720° of relative rotor rotation.

It should be noted that each individual thermodynamic cycle occurs over a period defined by 240° of relative rotor rotation, that is, 480° of piston rotation and 720° of

chamber rotation. Whichever component, whether the coupled pistons 2 and 5 or the coupled units 1 and 4 is employed as the engine work output medium or heat pump work input medium, the thermodynamic cycles have a longer duration than those occurring in conventional reciprocating heat engines and reciprocating heat pumps. These must, perforce, occur over 360° of the output, or input, shaft rotation. This feature of the rotary machine described above allows enhanced heat transfer processes, enabling the theoretically ideal thermodynamic cycle to be approached.

In Figure 6, the two units 1 and 4 are rigidly coupled by a hollow shaft 13 journalled at 14 and 15 in a fixed mounting 16. The pistons 2 and 5 are carried by a common shaft 17 journalled at 18 and 19 in the mounting 16. The ports 7, 8, 9 and 10 are in the flat radial sides of the chambers 3 and 6, near their peripheries, and are open and closed by the flat faces of the pistons 2 and 5. A gear coupling 20 between the shafts 13 and 17 ensure that the units 1 and 4 rotate relatively to the pistons 2 and 5 in the manner described.

The units 1 and 4 can be encapsulated or shrouded to distinct upper and lower temperature regions around them, each unit presenting a large surface area for efficient heat transfer. The rotation of those units promotes near-uniform temperature distribution.

In addition to maintaining a temperature differential between the units 1 and 4, there can be additional heating and cooling means for the ducts 11 and 12 provided, for

example, by adaptation of the encapsulation or shrouding to enclose the ends of the ducts. Any further heating means will be between the regenerators and the unit 1, while any further cooling means will be between the regenerators and
5 the unit 4.

Figure 6 shows the two rotatable structures isolated, for simplicity. There will of course be a connection to one or the other in order to get work out, in the case of an engine, or to put work in, in the case of a pump. The
10 shafts 13 and 17 can be suitably adapted.

It will be understood that while a simple embodiment with three-sided pistons operating in two-lobed chambers has been described, there could be more elaborate arrangements with $n+1 (n>2)$ sided pistons in n -lobed chambers connected by
15 a corresponding number of ducts with regenerators. The relative speeds of rotation of the chambers to the pistons will be $n+1:n$.

TABLE I

Piston Rotation	Chamber Rotation	Relative Rotor Notation	Compression Chamber	Duct	Compression Chamber
0	0	0	3a	3c	11
		-	Expan	Exhaust	-
				Regen	Comp
				-	Intake
30	45	15	Intake	Exhaust	-
				Regen	Exhaust
				-	Intake
60	90	30	Expan	Exhaust	-
				Regen	Comp
				-	Intake
90	115	45	Expan	Exhaust	-
				Regen	Intake
				-	Intake
120	180	60	Expan	Exhaust	-
				Regen	Comp
				-	Intake
150	225	75	Expan	Exhaust	-
				Regen	Exhaust
				-	Intake
180	270	90	Expan	Exhaust	-
				Regen	Comp
				-	Intake
210	315	105	Exhaust	Expan	-
				Regen	Intake
				-	Intake
240	360	120	Exhaust	Expan	-
				Regen	Comp
				-	Intake
270	405	135	Exhaust	Intake	-
				Regen	Exhaust
				-	Intake
300	450	150	Exhaust	Expan	-
				Regen	Comp
				-	Intake
330	495	165	Exhaust	Expan	-
				Regen	Intake

Rotation angles are in degrees.

Expan : an Expansion process.

Regen : Regenerative transfer from expander to compressor.

→ Regen : Regenerative transfer from compressor to expander.

- : stagnated fluid or vapour flow.

Comp : a compression process.

TABLE I (Cont'd)

Piston Rotation	Chamber Rotation	Relative Rotor Rotation	Compression Chamber			Duct	Compression Chamber		
			3a	3b	3c		11	12	6a
360	540	180	-	Expan	Exhaust	-	→ Regen	Comp	Comp
390	585	195	Intake	Expan	Exhaust	← Regen	Regen	Comp	Intake
410	630	210	Expan	Expan	Exhaust	-	→ Regen	Comp	Intake
450	675	225	Expan	Exhaust	Exhaust	→ Regen	Regen	Comp	Intake
460	720	240	Expan	Exhaust	-	→ Regen	-	Comp	Comp
510	765	255	Expan	Exhaust	Intake	→ Regen	Regen	Exhaust	Intake
540	810	270	Expan	Exhaust	Expan	→ Regen	-	-	Intake
570	855	285	Exhaust	Expan	Expan	→ Regen	Regen	Intake	Intake
600	900	300	Exhaust	-	Expan	-	→ Regen	Intake	Comp
630	945	315	Exhaust	Intake	Expan	→ Regen	Regen	Intake	Comp
660	590	330	Exhaust	Expan	Expan	-	→ Regen	Intake	Comp
690	1035	345	Exhaust	Expan	Exhaust	→ Regen	Regen	Intake	Comp
720	1080	360	-	Expan	Exhaust	→ Regen	-	Comp	Intake

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TABLE 2

%	30/45	69/40	90/135	149/90	159/215	160/210	210/135	240/360	270/450	307/450	339/415	365/540
	Comp	6a			Regen	6a + Duct 11 + 3c		Expan	3c	3c + Duct 12 + 3c	Regen	

360/550	310/555	420/630	155/725	490/720	510/615	540/810	570/635	605/800	630/645	660/610	695/555	720/600
	Regen	3c + Duct 12 + 6c]			Comp	6c		Regen	11 + 3b	6c + Duct 11 + 3b	Expan	3b

715/630	755/715	810/710	810/215	840/740	870/705	900/750	930/815	960/840	990/935	1020/970	1050/1025	1150/1120
	Expan	3b			Regen	Duct 15 + 6b				Comp	6b	

1080/120	1110/1155	1140/110	1170/1155	1200/960	1230/945	1270/930	1290/915	1310/960	1350/925	1380/920	1410/915	1440/910
	Regen	6b + Duct 11 + 3b		Expan	3a				Regen	12 + 6a		

Numbers denote the piston rotation followed by the corresponding chamber rotation in degrees.

Comp : Compression process. Regen : Regenerative transfer process.

Expan : Expansion process. 6a, 6b, 6c: compression chamber identification.

Claims

1. A fluid or vapour rotary piston machine including two variable-volume units, each unit having a rotary multi-lobed epitrochoidal chamber and a multi-sided rotary piston therein forming a plurality of individual sub-chambers by its co-operation with the periphery of the associated chamber, the number $(n+1)$ of piston sides being greater by one than the number (n) of epitrochoid arcs, wherein the two chambers are constrained to rotate at a first common speed about a first effective common axis while the two pistons are constrained to rotate at a second common speed about a second effective common axis, the ratio of first to second common speeds being $n+1:n$, wherein each chamber has a plurality (n) of dual-function ports enabling connection between the chambers via ducts, and wherein said ducts each contain a regenerator, enabling one variable-volume unit to perform intake, expansion and exhaust, while the other unit performs intake, compression and exhaust, as a result of the relative rotation and port positions.

2. A rotary piston machine as claimed in claim 1, wherein heating means are provided for the variable-volume unit which performs the expansion processes.

3. A rotary piston machine as claimed in claim 2, wherein further heating means are provided between each said regenerator and the variable-volume unit which performs the expansion processes.

4. A rotary piston machine as claimed in claim 1, 2 or 3, wherein cooling means are provided for the variable-

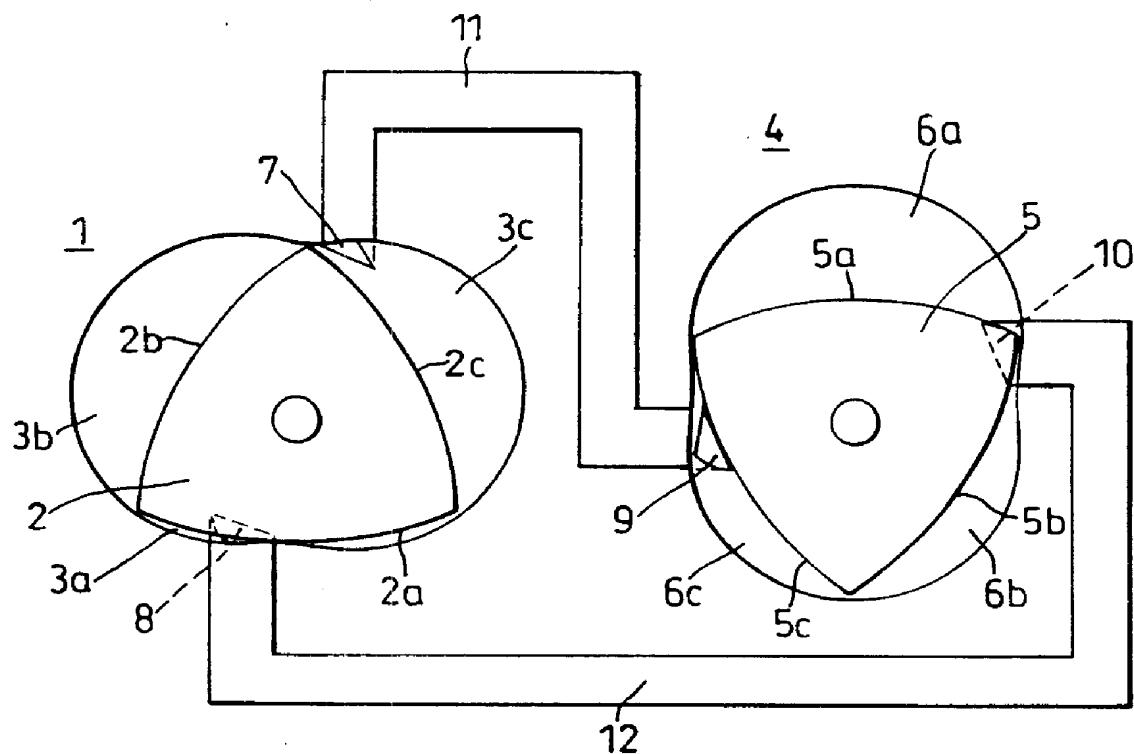
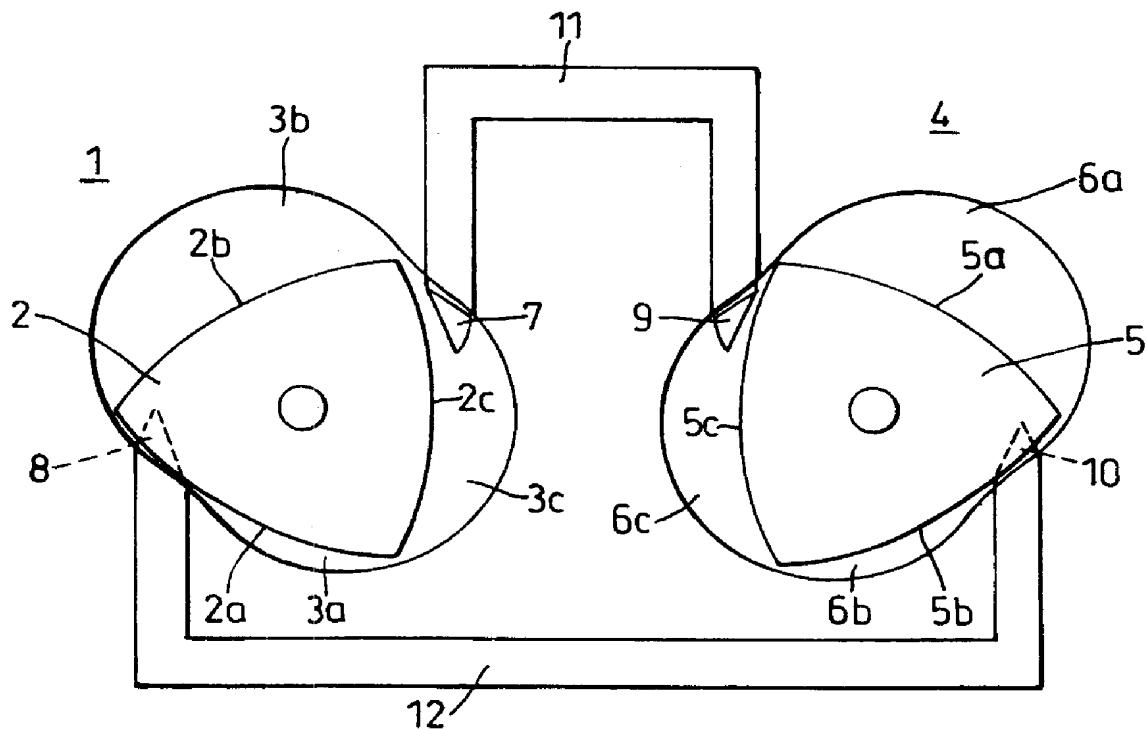
volume unit which performs the compression processes.

5. A rotary piston machine as claimed in claim 4,
wherein further cooling means are provided between each said
regenerator and the variable-volume unit which performs the
5 compression processes.

6. A rotary piston machine as claimed in any
preceding claim, wherein n=2.

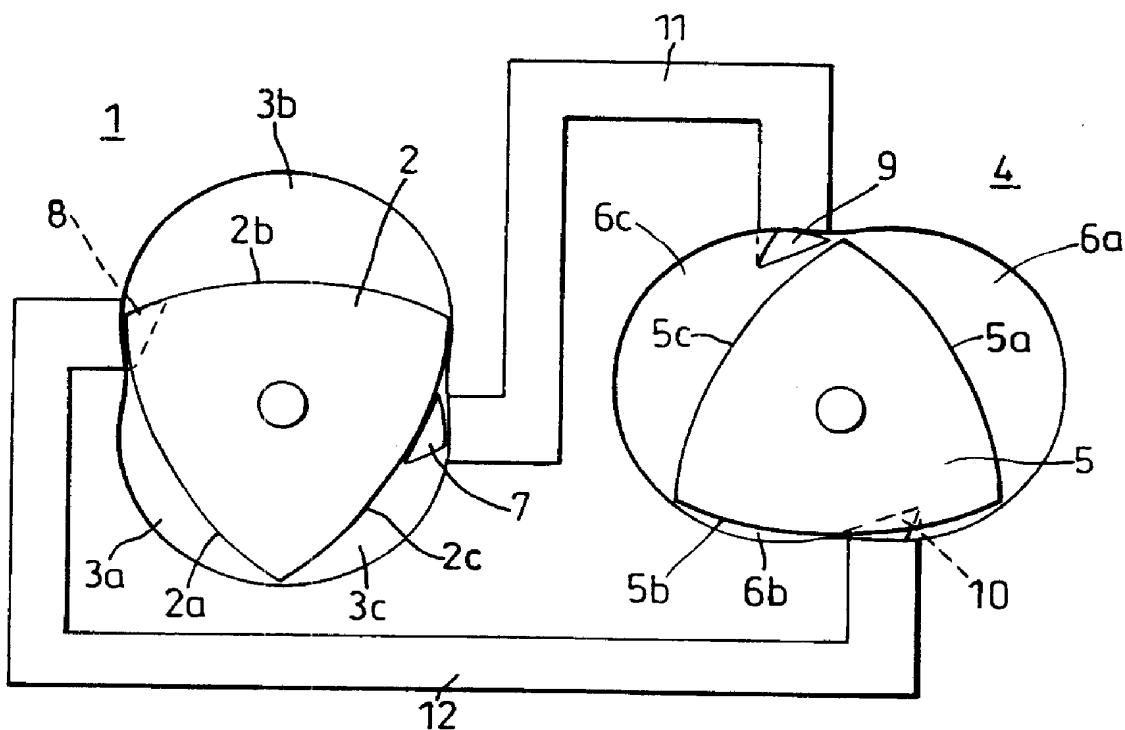
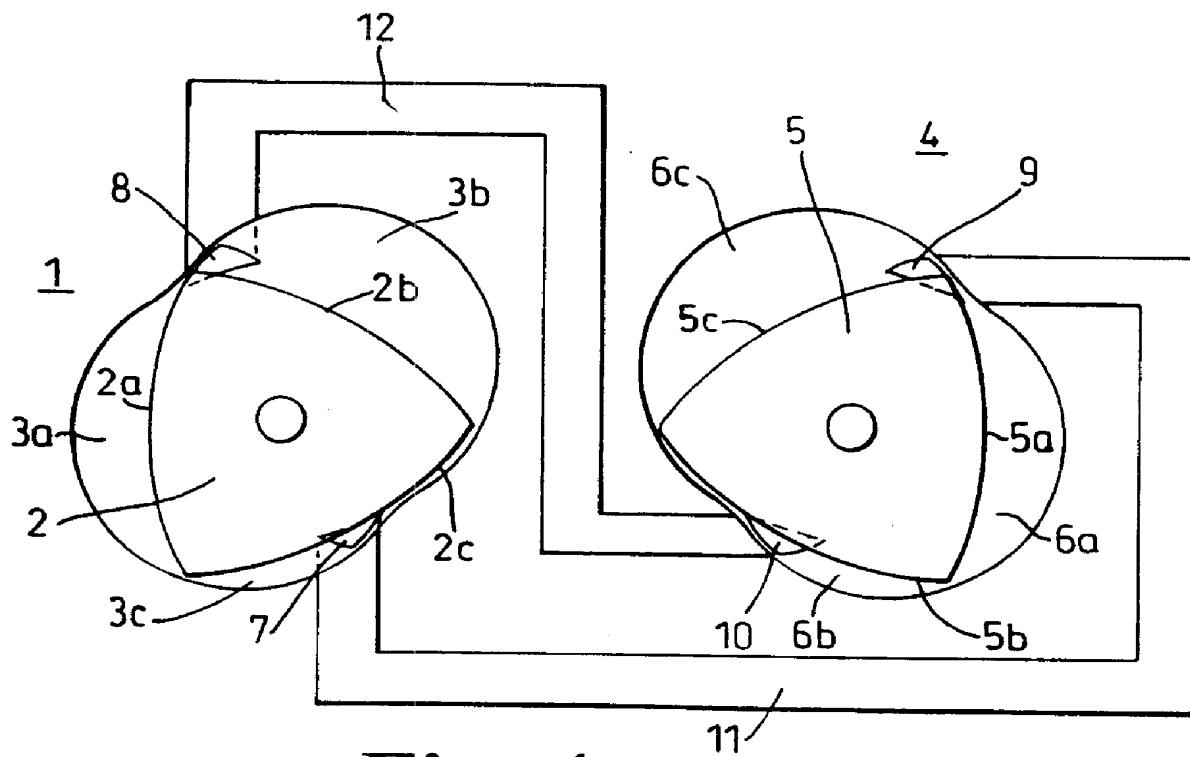
7. A rotary piston machine substantially as
hereinbefore described with reference to the accompanying
10 drawings.

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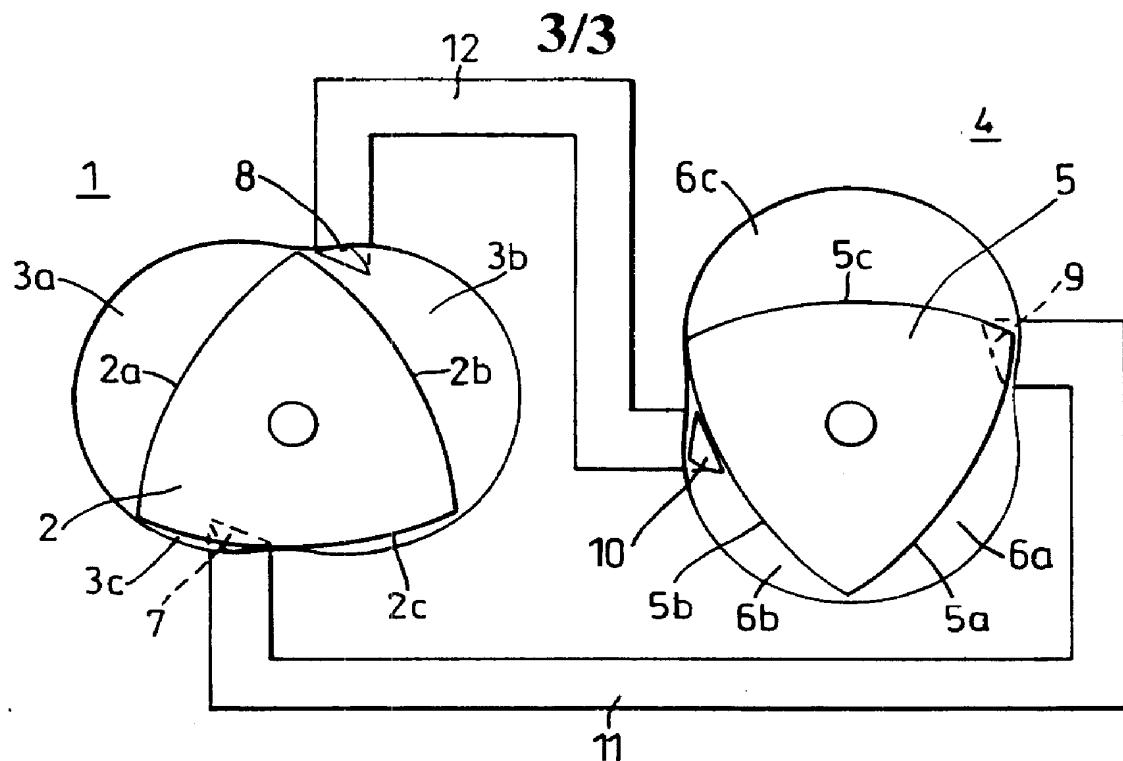
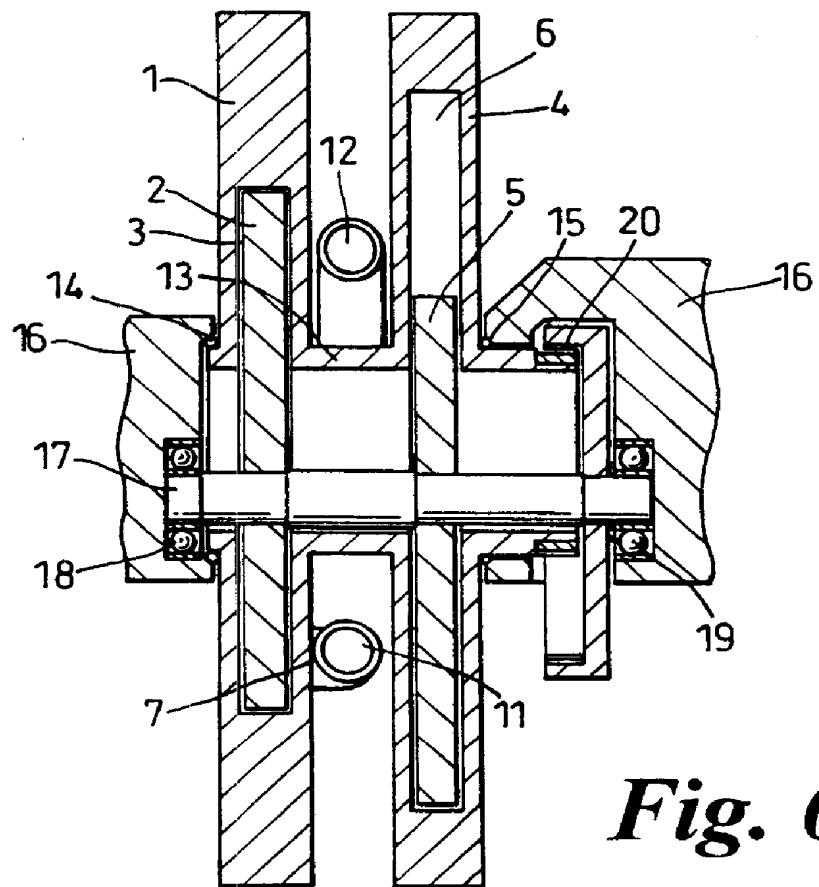
*Fig. 1**Fig. 2*

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*Fig. 3**Fig. 4*

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*Fig. 5**Fig. 6*

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INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 99/01290

A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 F02G1/043 F01C11/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 F02G F01C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 3 744 940 A (PIERCE E ET AL) 10 July 1973 (1973-07-10) figures 10-12 abstract column 4, line 4 - line 53 ----	1,6,7
A	figures 10-12 abstract column 4, line 4 - line 53 ----	2,4
Y	US 5 251 596 A (WESTLAND MARTIN W) 12 October 1993 (1993-10-12) figures 1,2,4 abstract column 5, line 19 - line 42 ----	1,6,7
A	US 3 763 649 A (BRAUN E ET AL) 9 October 1973 (1973-10-09) figure 1 abstract column 2, line 23 - line 58 ----	1,7
		-/-

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

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Date of the actual completion of the international search

Date of mailing of the international search report

9 July 1999

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Name and mailing address of the ISA

European Patent Office, P.B. 5618 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

Wassenaar, G

INTERNATIONAL SEARCH REPORT

International Application No
PCT/GB 99/01290

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5 410 998 A (PAUL MARIUS A ET AL) 2 May 1995 (1995-05-02) figure 2 abstract column 5, line 37 - column 6, line 37 -----	1-3,6,7

INTERNATIONAL SEARCH REPORT

Information on patent family members

Int.	International Application No.
	PCT/GB 99/01290

Patent document cited in search report	Publication date	Patent family member(s)		Publication date
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